



51-135311

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My commission expires March 25, 1994



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Notary Public

19. Japan Patent Office (JP)

11. Patent publication
Sho 51-133311

43. Announcement date November 19, 1976

51. Int. Cl ⁴	Identification code	Internal management code
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C03C 3104		741741
C03C 3130		
C03C 13100		

52. Japan classification 21 A23

Inspection requests - not requested
Total number of inventions 1 (total of five pages)

1. Invention title - glass composition for use as glass fibers

(21) Application Sho 50-56706
(22) Date of application May 15, 1975

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5. List of attachments
(1) Detail [illegible] one
(2) ----

- (3) Power of attorney, one supplemental attachment
(4) Supplement to application: one

1. Title of the invention

Glass composition for use as glass fibers

2. Range of patent application claims

The compositions contains the following.

SiO ₂	35 - 75% by weight
Al ₂ O ₃	1 - 25% by weight
CaO	23 - 63% by weight
MgO	1 - 10% by weight
Fe ₂ O ₃	0 - 1.5% by weight
R ₂ O	0 - 10% by weight
X	0 - 5% by weight

The proportion of SiO₂ is limited to a maximum of 30% but the ZrO₂ can be [illegible]; the R₂O is selected from among the group K₂O, Na₂O, and Li₂O. The X is selected from among the group ZnO, BaO, SrO, TiO₂, Al₂O₃, Sb₂O₃, F, and SO₃. The constituents above constitute 99% or more by weight of the cement material used to form the glass fiber composition.

3. Detailed description of the invention

This invention is of a glass composition with glass fibers; the composition is highly alkali-resistant.

In existing technology, the cement material [illegible] is strengthened and [illegible]. Also, a strengthening cement is used with fibers that are themselves strong. Asbestos was once used for these strong fibers.

However, in recent years asbestos has become an environmental problem. Use has declined to the point that its use as a resource is no longer a problem, but only a few materials have properties that are equal or superior to asbestos. Glass fiber is one of those materials, and the use of glass fiber is becoming more widespread.

Most glass fibers have SiO₂ as the main constituent, with ZrO₂, SnO, or TiO₂ added to improve alkali-resistance properties or CaO, MgO, or Al₂O₃ added, also to improve alkali-resistance properties, resulting in two main types of glass fibers.

Among the glass fiber constituents named above, ZrO_2 improves alkali-resistance properties the most markedly, but it also results in glass fibers with poor fusibility, and they de-vitrify easily. The constituents of the glass fibers include up to 20% by weight. The inclusion of 10 - 20% by weight leads to a number of problems but the alkali resistance is poor if less than 10% by weight is included.

Also, the previously noted main constituent of SiO_2 can be used in making glass fibers with a high proportion of Al_2O_3 , MgO , or CaO , but the resulting glass fibers also have poor fusibility and de-vitrify easily, problems identical with those found in high ZrO_2 glass, making them difficult to [illegible].

In comparison with the types of glass described above, this invention includes SiO_2 , MgO , and CaO as mandatory constituents. The resulting glass compound has both a high resistance to alkalis and excellent fusibility. The constituents are as follows.

SiO_2	35 - 75% by weight
Al_2O_3	1 - 25% by weight
CaO	23 - 63% by weight
MgO	1 - 10% by weight
Fe_2O_3	0 - 1.5% by weight
R_2O	0 - 10% by weight
X	0 - 5% by weight

The proportion of SiO_2 is limited to a maximum of 30% but the ZrO_2 can be [illegible]; the R_2O is selected from among the group K_2O , Na_2O , and Li_2O . The X is selected from among the group ZnO , BaO , SrO , TiO_2 , Al_2O_3 , Sb_2O_3 , F, and SO_3 . The constituents above constitute 99% or more by weight of the cement material used to form the glass fiber composition.

The glass composition that is the subject of this invention has high alcohol-resistance properties and good fusibility. It is comparatively hard to de-vitrify, and as its [illegible] is also good it is [largely illegible - probably "comparatively easy to work"]. Its resistance to alkalis means that a strongly alkali cement can be added to the mixture and used for long periods of time.

With regard to this invention, the percentage by weight of SiO_2 is to be 35 - 75%. If the content is less than 35%, vitrification difficult, the liquefaction is poor, and the conversion into fibers is a problem. On the other hand, if the content is more than 75%, the resistance to alkalis is a problem and difficulties with conversion into fibers emerge.

The middle range of 40 - 65% by weight is especially favorable. For alkali-resistant properties and for conversion into fibers the range of 40 - 56% by weight is most desirable.

Also, even though the maximum amount of SiO_2 is 30% by weight (ratio of SiO_2 in the mixture) and ZrO_2 is [illegible], neither the alkali resistance nor the liquefaction properties show difficulties.

The amount of Al_2O_3 is to be 1 - 25% by weight. Liquefaction becomes poor if it is less than 1% by weight, and if it is more than 25% by weight the resistance to alkalis is degraded. Alkali resistance is best in the middle range of 20% by weight or less.

The amount of CaO is to be 23 - 63% by weight. Alkali resistance is degraded if it is less than 23% by weight. If it is more than 63%, liquefaction becomes poor and conversion into fibers is a problem. In the middle range of 32 - 50% by weight, though, particularly in the range of 35 - 50%, both resistance to alkalis and liquefaction are good.

The amount of MgO is to be 1 - 10% by weight. If it is less than 1% or more than 10% the liquefaction is poor. The middle range of 2 - 8% by weight results in ease of [illegible].

The amount of Fe_2O_3 is to be 0 - 1.5% by weight. The role of this constituent is to improve liquefaction, but if the amount present is more than 1.5% by weight, it has an adverse effect on the resistance to alkalis.

R_2O is to be chosen from among the group K_2O , Na_2O , and Li_2O and is to constitute 0 - 10% by weight. This constituent is meant to aid liquefaction, but if it constitutes more than 10%, the [illegible] is poor. The best range for this constituent is 0 - 5% by weight.

X is to be chosen from among the group ZnO , BaO , SrO , TiO_2 , Al_2O_3 , Sb_2O_3 , F, and SO_3 . The main purpose of this constituent is to aid liquefaction. The amount used for that purpose is 0 - 5% by weight. If more than 5% is used, the resistance to alkalis is adversely affected.

These constituents constitute 99% or more by weight. It is possible for the constituents described above whose purpose is to improve liquefaction to make up less than 1% by weight of the total.

A good proportion of ingredients for this invention is shown below.

SiO_2	40 - 65% by weight
Al_2O_3	1 - 20% by weight
CaO	32 - 50% by weight
MgO	2 - 6% by weight
Fe_2O_3	0 - 1.5% by weight
R_2O	0 - 10% by weight
X	0 - 5% by weight

The proportion of SiO_2 is limited to a maximum of 30% but the ZrO_2 can be [illegible]; the R_2O is selected from among the group K_2O , Na_2O , and Li_2O . The X is selected from among the group ZnO , BaO , SrO , TiO_2 , Al_2O_3 , Sb_2O_3 , F, and SO_3 . The constituents above constitute 99% or more by weight of the cement material used to form the glass fiber composition.

Particularly effective ranges for this patent are shown below.

SiO_2	40 - 56% by weight
Al_2O_3	1 - 20% by weight
CaO	35 - 50% by weight
MgO	2 - 8% by weight
Fe_2O_3	0 - 1.5% by weight
R_2O	0 - 5% by weight
X	0 - 5% by weight

The proportion of SiO_2 is limited to a maximum of 30% but the ZrO_2 can be [illegible]; the R_2O is selected from among the group K_2O , Na_2O , and Li_2O . The X is selected from among the group ZnO , BaO , SrO , TiO_2 , Al_2O_3 , Sb_2O_3 , F, and SO_3 . The constituents above constitute 99% or more by weight of the cement material used to form the glass fiber composition.

The process of forming the glass compound used in this invention involves liquefying the raw materials together in fixed amounts and passing them through an orifice, extruding them; the rotator with many [illegible, possibly "caps"] to which the orifices are attached is supplied [with the raw material] and rotated at a high-speed rotation, centrifugal force causes the glass to flow from the orifice and to be dispersed. A high-temperature gas heater is used in drawing the glass. The glass flow is warmed by the gas heater and dispersed, becoming the glass [fibers] used in the next stage of production.

Next, application examples No. 1 through No. 11 and comparison examples No. 12 through No. 17, shown in Tables 1 through 3, are described.

The test of alkali resistance involves boiling a sample in an aqueous 1N-NaOH solution for one hour, letting it stand for six hours, washing it and drying it, then comparing the weight of the sample with the weight of an untreated sample to determine the amount by which the weight was reduced.

In addition, with regard to the liquefaction properties (particularly liquefaction at a given temperature), an attempt was made to liquefy the base materials completely. Those that showed good liquefaction are given the designation A; those for which a considerable [illegible, possibly "rise in temperature"]

was necessary are given the designation B; those for which liquefaction and conversion to glass fibers posed problems are given the designation C.

Table 1

	No. 1	No. 2	No. 3	No. 4	No. 5	No. 6
SiO ₂	42	40	50	68	50	40
ZrO ₂	--	5	2	--	--	5
SnO ₂	--	0.5	--	--	--	0.5
TiO ₂	--	--	--	0.5	--	--
CaO	40	37	34	24	30	30
MgO	5	4	6	2	7	8
BaO	--	--	1	--	1	--
ZnO	--	--	--	--	--	0.5
SrO	--	1	0.5	--	--	--
K ₂ O	--	1	--	--	--	--
Na ₂ O	--	--	0.5	0.5	1	0.5
Li ₂ O	--	--	--	--	0.5	--
Al ₂ O ₃	13	11	6	5	10	14
Fe ₂ O ₃	--	0.3	--	--	--	1
As ₂ O ₃	--	--	--	--	0.4	--
Sb ₂ O ₃	--	--	--	--	--	0.3
B ₂ O ₃	--	--	--	--	--	--
F	--	--	--	--	0.1	--
SO ₃	--	--	--	--	--	0.2
Liquefaction properties	A	A	B	B	A	A
alkali resistance properties mg/cm ²	0.0030	0.0025	0.0060	0.0095	0.0075	0.0068

Table 2

	No. 7	No. 8	No. 9	No.10	No. 11
SiO ₂	50	37	42	40	48
ZrO ₂	5	--	0.5	--	0.5
SnO ₂	--	--	0.5	--	--
TiO ₂	--	--	--	--	--
CaO	30	38	48	42	40
MgO	5	2	5	6	6
BaO	--	00	0.5	--	--
ZnO	--	0.5	--	--	--
SrO	--	--	--	1	--
K ₂ O	--	--	--	0.5	--
Na ₂ O	--	--	0.5	--	--
Li ₂ O	--	--	--	--	0.5
Al ₂ O ₃	10	21	3	10	5
Fe ₂ O ₃	--	1.2	--	--	--
As ₂ O ₃	--	1.3	--	--	--
Sb ₂ O ₃	--	--	--	--	--
B ₂ O ₃	--	--	--	--	--
F	--	--	--	--	--
SO ₃	--	--	--	0.5	--
Liquefactio n properties	A	A	A	A	A
alkali resistance properties mg/cm ²	0.0110	0.0080	0.0050	0.0055	0.0032

Table 3

	No. 12	No. 13	No. 14	No.15	No. 16	No. 17
SiO ₂	45	30	40	64	45	54

ZrO ₂	--	--	--	--	--	--
SnO ₂	--	--	--	--	--	--
TiO ₂	--	--	--	--	--	0.2
CaO	40	57	28	20	38	17.5
MgO	2	3	4	5	--	4
BaO	--	--	--	--	--	--
ZnO	--	--	--	--	--	--
SrO	--	--	--	--	--	--
K ₂ O	--	--	--	--	--	--
Na ₂ O	0.3	--	--	--	--	0.3
Li ₂ O	--	--	--	--	--	--
Al ₂ O ₃	10	10	28	11	17	14
Fe ₂ O ₃	2.5	--	--	--	--	--
As ₂ O ₃	--	--	--	--	--	--
Sb ₂ O ₃	--	--	--	--	--	--
B ₂ O ₃	--	--	--	--	--	10
F	--	--	--	--	--	--
SO ₃	--	--	--	--	--	--
Liquefaction properties	A	C	A	C	C	A
alkali resistance properties mg/cm ²	0.0030	0.0025	0.0060	0.0095	0.0075	0.0068

All of application examples No. 1 through No. 11 showed excellent resistance to alkali and excellent liquefaction properties. Compared to the E-glass of No. 17, the alkali resistance results show a loss weight at a level 2/3 or less than the loss seen in No. 17. No. 1, No. 2, and No. 11, in particular, show good resistance to alkalis, with a loss of weight 1.6 that of No. 17.

Also, No. 12 the example that contains 2.5% by weight of Fe₂O₃, shows good liquefaction but lowered resistance to alkalis.

No. 13 is the example that contains a small amount of SiO₂,

30% by weight. Liquefaction properties are lowered, the conversion of the glass into fibers is difficult, and the resistance to alkalis is lowered.

No. 14, in which the amount of Al_2O_3 is a high 28% by weight, shows good liquefaction but resistance to alkalis is lowered.

No. 15, in which the amount of CaO is a scant 20% by weight, and No. 16, which has no MgO , both have good resistance to alkalis but the liquefaction properties are lowered and conversion into fibers is a problem.

As noted before, No. 17 is E-glass. It has good liquefaction properties but resistance to alkalis is a problem.

Among the application examples of this invention. Nos. 1, 2, 3, 9, 10, and 11 have the most desirable selection of constituents. They show a loss of weight due to alkali action that is $1/3$ or less than the loss seen in E-glass. all of the examples in the desirable range, Nos. 1, 2, 3, 9, 10, and 11, show good liquefaction properties. In particular Nos. 1, 2, and 11 show a loss of weight due to alkali action that is $1/6$ or less than the loss seen in E-glass.

This invention thus improves the alkali resistance and liquefaction properties of glass composition, and when fibers are produced by the method outlined above the fibers are long and can be gathered into stranded bundles. Strands can be cut or uncut, and cements with alkali properties such as Portland cement, aluminum cement, the cement used with asbestos can be used with these glass fibers.

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り、10～20 wt% 含有する場合にはガラスの
強度が多く、又10 wt% 未満においては、苛
性アルカリ性が劣ってくるという問題を引
起していた。

又、従 前、 SiO_2 を主成分とし、 Al_2O_3
のガラス成分に MgO のガラス、或いは CaO
のガラスをばらばら添加されているが、三酸塩
化を多く、安定しやすいたの成分の ZrO_2 の
割合と肉質に改良化しにくく、作製性を悪くし
ていた。

本発明は、前述のガラスの肉質を改善し、
 SiO_2 、 Al_2O_3 、 CaO 、 MgO を主成分とし、
残れた苛性アルカリ性を有し、かつ耐熱性にも改
良したガラス組成物を目的としたものであり、

SiO_2	35～75 wt%
Al_2O_3	1～25 wt%
CaO	23～63 wt%
MgO	1～10 wt%
Fe_2O_3	0～1.5 wt%
R_2O	0～10 wt%
X	0～5 wt%

アルカリ性と、改良化の作製性の面からみて40
～56 wt% とすることが好ましい。又、 SiO_2
は、その含有量の肉質大は30 wt% (SiO_2 の
含有量に比し)を ZrO_2 に改良しても、苛アル
カリ性、耐熱性上問題はない。

Al_2O_3 は1～25 wt% であり、1 wt% 未満に
おいては耐熱性が悪くなり、改良化が困難であ
り、25 wt% より多数の場合においては、苛ア
ルカリ性の劣化が避けにくく、中でも20 wt%
以下とする方が苛アルカリ性上好ましい。

CaO は23～63 wt% であり、23 wt% 未満
においては苛アルカリ性が劣り、23 wt%
より多数の場合においては、耐熱性が悪くなり、
改良化が困難となる。中でも32～50 wt%、
特に35～50 wt% とすることにより苛アルカ
リ性、耐熱性とも良好となる。

MgO は1～10 wt% であり、1 wt% 未満又は10
wt% より多数の場合においては耐熱性が悪化し
好ましくなく、中でも2～8 wt% とすることによ
り改良化しやすくなる。

であり、この肉 SiO_2 の肉質大は30 wt% まで
 ZrO_2 で改良可能であり、 R_2O は Li_2O 、 Na_2O 、
 Li_2O の群から選ばれ、X は ZnO 、 BaO 、 SrO 、
 TiO_2 、 Ag_2O_3 、 Sr_2O_3 、 Zr 、 Sn の群から選
ばれ、上記の成分の含有率が99 wt% 以上であ
るモノトム改良化性ガラス組成物を表すであ
る。

本発明のガラス組成物は、苛性アルカリ性を
有しており、耐熱性も高く、安定化も比較的
しやすく、かつ肉質にも改良されているため改良
しやすく、改良性がよい上に苛性アルカリ性を
有するモノトム改良化に導入しても改良化のた
り高い改良能力を有するものである。

本発明においては、 SiO_2 は35～75 wt%
であり、35 wt% 未満においては、ガラス化し
にくく、耐熱性が悪くなり、改良化が困難であ
り、25 wt% より多数の場合においては苛
アルカリ性上に問題がでてくるとともに改良化
が困難となる。

中でも40～65 wt% 程度に改良して残れた苛

Fe_2O_3 は0～1.5 wt% であり、耐熱性を改良
する成分であるが、苛アルカリ性の面からみて
1.5 wt% より多数になると好ましくない。

R_2O は Li_2O 、 Na_2O 、 Li_2O の群の中から選
ばれ、耐熱性を改良する成分で、0～10 wt%
であり、10 wt% より多数になると、苛
性性が悪化してくるため好ましくなく、特に0
～5 wt% とすることが好ましい。

X は ZnO 、 BaO 、 SrO 、 TiO_2 、 Ag_2O_3 、 Sr_2O_3 、 Zr
の群から選ばれる成分であり、主として耐熱性
を改良するために使用され0～5 wt% であり、
5 wt% より多数の場合においては、苛アルカリ
性を悪化させるため好ましくない。

そして、これらの含有率が99 wt% 以上であり、
上記成分の群に、耐熱性を改良するための肉質の
改良成分は不純物を1 wt% 未満であつたまま
有しても使用できる。

以下、本発明の好ましい組成は、

SiO_2	40～65 wt%
Al_2O_3	1～20 wt%

SiO ₂	40-56	wt%
Al ₂ O ₃	1-20	wt%
CaO	35-50	wt%
MgO	2-8	wt%
Fe ₂ O ₃	0-1.5	wt%
SrO	0-5	wt%
X	0-5	wt%

を以て、四角形のX量と比較してその減量を測定して行なつた。

又、組織性は、組織抵抗（特定組織にのみある抵抗）、或種の完全組織に於ける時、組織化の目的に於てより必要をなし、是所のものを、若干修正を加ふ必要なるものを、作用の目的たるもの及び組織化の爲めに組織たるものをとした。

であり、この内 SiO_2 の内訳は SiO_2 として
 SiO_2 、 Si_2O_5 、 Si_3O_8 であり、 SiO_2 は SiO_2 、 Si_2O_5 、
 Si_3O_8 の群から成られ、 Si_2O_5 、 Si_3O_8 、 SiO_2 、
 SiO_2 、 Al_2O_3 、 Si_2O_5 、 Si_3O_8 の群から成
 られ、上述の色表示の含有 SiO_2 99.9%以上である
 を示す試験成績は、 SiO_2 は SiO_2 、 Si_2O_5 、 Si_3O_8 である。

この時のガラス管は、全長約二メートルに達して居りし程度をセキツイスに切りガラス管として用ひられ、高圧密着している部分のセキツイスを多量とするカップ材の密着は不十分で、お心力により割裂のセキツイスから細いガラス管として抜けされ、高圧ガス装置より送附されて遠方のガラス管として回収される、大いにガラス管を製造設備にロスした事で損失を増しては損耗ガラス管として処理される。

及び此等式(12) - (17) を用いて計算する。

たし、 Al^{3+} カリシの生成は、1% NaOH 水溶液にて1時間放置処理し、6時間放置後、水に

	A 1	A 2	A 3	A 4	A 5	A 6
SiO ₂	4.2	4.0	5.0	6.8	5.0	4.0
ZrO ₂	—	5	2	—	—	5
SnO ₂	—	0.5	—	—	—	0.5
TiO ₂	—	—	—	0.5	—	—
CaO	4.0	3.7	3.4	2.4	3.0	3.0
MgO	5	4	6	2	7	6
NaO	—	—	1	—	1	—
ZnO	—	—	—	—	—	0.5
FeO	—	1	0.5	—	—	—
K ₂ O	—	1	—	—	—	—
Na ₂ O	—	—	0.5	0.5	1	0.5
Li ₂ O	—	—	—	—	0.5	—
Al ₂ O ₃	1.3	1.1	6	5	1.0	1.4
P ₂ O ₅	—	0.5	—	—	—	1
As ₂ O ₃	—	—	—	—	0.4	—
Sb ₂ O ₃	—	—	—	—	—	0.3
B ₂ O ₃	—	—	—	—	—	—
F	—	—	—	—	0.1	—
SO ₃	—	—	—	—	—	0.2

化学式	A	A	B	B	A	A
HTA-052	00030	00025	00060	00095	00075	00066
95/100						

	А 7	А 8	А 9	А 10	А 11
SiO ₂	50	37	42	40	48
ZrO ₂	5	—	0.5	—	0.5
SnO ₂	—	—	0.5	—	—
TiO ₂	—	—	—	—	—
CaO	30	38	48	42	40
HgO	5	2	5	6	6
BaO	—	—	0.5	—	—
ZnO	—	0.5	—	—	—
SrO	—	—	—	1	—
K ₂ O	—	—	—	0.5	—
Na ₂ O	—	—	0.5	—	—
Li ₂ O	—	—	—	—	0.5
Al ₂ O ₃	10	21	3	10	3
Fe ₂ O ₃	—	1.2	—	—	—
As ₂ O ₃	—	0.3	—	—	—
SnO ₃	—	—	—	—	—
B ₂ O ₃	—	—	—	—	—
F	—	—	—	—	—
SO ₃	—	—	—	0.5	—

А 7	А 8	А 9	А 10	А 11
00110	00080	00050	00055	00032

	A12	A13	A14	A15	A16	A17
SiO ₂	45	30	40	64	45	34
ZrO ₂	-	-	-	-	-	-
SnO ₂	-	-	-	-	-	-
TiO ₂	-	-	-	-	-	0.2
CaO	40	57	28	20	38	17.5
MgO	2	3	4	5	-	4
3Al ₂ O ₃	-	-	-	-	-	-
ZnO	-	-	-	-	-	-
FeO	-	-	-	-	-	-
K ₂ O	-	-	-	-	-	-
Na ₂ O	0.5	-	-	-	-	0.3
Li ₂ O	-	-	-	-	-	-
Al ₂ O ₃	10	10	28	11	17	14
P ₂ O ₅	2.5	-	-	-	-	-
As ₂ O ₃	-	-	-	-	-	-
Sb ₂ O ₃	-	-	-	-	-	-
B ₂ O ₃	-	-	-	-	-	10
F	-	-	-	-	-	-
SO ₃	-	-	-	-	-	-
其他	A	C	A	C	C	A
778990	00135	0148	00132	00102	001110	00190
g/d						

表 4. 例 4. $\alpha = 1$ は、いつでも使れた射 τ の α カリ性と局所性を有しており、 $\alpha = 1$ を示したところと比べて $\frac{2}{3}$ 以下、 $\alpha \leq 1$ 、 $\alpha = 2$ 、 $\alpha = 1$ 等では $\frac{1}{6}$ 程度の α カリ性による減少しか認められなく、局所性も良いものである。

又、 μ_{12} は、 F_{103} を 2.5 倍増強したものであり、 μ_{12} の値が好であるが前アムリヒが低下している。

、13は、510が30程度と少ないのであり、反応性が低下し、塩化が極めて遅減となり、かつ新アムカサ性も低下している。

成 1.4%、 Al_2O_3 が 2.8% と多い所であり、
耐酸性は良好であるが、耐アルカリ性は低下し
ている。

▲ 15 は、 CaO が 20 wt% と少ない例であり、
▲ 16 は MgO が 0 wt% の例であり、 Fe 、 K 、 F 、 Al
カリウム、鉄、フッ素と示えるが、 Fe 、 K 、 F が盛のて低下
して、 Al の酸化が原因となつてゐる。

ル１？は前述の如く「エーダス」であり、後編世
は風竹であるが新アムカリ位の風で問題となる。

たか本¹の $\bar{A}1$ 、 $\bar{A}2$ 、 $\bar{A}3$ 、 $\bar{A}9$ 、 $\bar{A}10$ 、 $\bar{A}11$ は好ましい組出の面であり、 $\bar{A}4$ より劣る面は E -ガラスに比し $\frac{1}{3}$ 以下となっており、さらに好ましい組出である $\bar{A}1$ 、 $\bar{A}2$ 、 $\bar{A}9$ 、 $\bar{A}10$ 、 $\bar{A}11$ においては、 $\bar{A}1$ 、 $\bar{A}2$ 、 $\bar{A}11$ は前述の如く E -ガラスに比し、 $\bar{A}4$ より劣る減量が $\frac{1}{6}$ 以下という優れたものである。

このように不発明のガラス管管端は封れたがアルカリ性と、腐蝕性を示し、前述の如き原因により管端部として、又は封の管端により長延縮若しくは長短縮を以て不純質したストランドとして、或いは長短縮、ストランドを切断して若しくは切断しないでマフトラに接合したマフトラとして、或いは管端として、又はこれらの管端部、管端部としてボルトランドセメント、アルミナセメント、石膏等質性アルカリ性のセメント質材料に投入して使用するのに従っている。

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